## Numerical Solutions of Partial Diffirential Equations

Thu Huyen Dao

25 November 2013

Thu Huyen Dao Numerical Solutions of Partial Diffirential Equations

(4月) (4日) (4日)

## Table of contents



2 Numerical Scheme



Thu Huyen Dao Numerical Solutions of Partial Diffirential Equations

- 4 回 2 - 4 □ 2 - 4 □

## Table of contents



2 Numerical Scheme



- - 4 回 ト - 4 回 ト



Figure: Pressurized Water Reactor

< □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □

## Table of contents







- - 4 回 ト - 4 回 ト

## Finite volume discretisation

$$\frac{\partial U}{\partial t} + \nabla \cdot (\mathcal{F}(U)) = 0 \tag{1}$$

Integrating (1) over  $C_i$ 

$$\frac{\partial}{\partial t} \left( \int_{C_i} U(x,t) \, \mathrm{d}\vec{x} \right) + \sum_{j \in N(i)} \int_{\partial C_{ij}} \mathcal{F}(U) \cdot \vec{n_{ij}} \, \mathrm{d}s = 0 \qquad (2)$$

Set  $U_i(t) = \frac{1}{v_i} \int_{C_i} U(x, t) dx$ , we have  $\frac{\partial}{\partial t} \left( \int_{C_i} U(x, t) d\vec{x} \right) \cong v_i \frac{\partial U_i(t)}{\partial t} \cong v_i \frac{U_i^{n+1} - U_i^n}{\Delta t}$ 

- 4 同 6 4 日 6 4 日 6

3

## Finite volume discretisation

We obtain the numerical scheme

$$\frac{U_i^{n+1} - U_i^n}{\Delta t} + \sum_{j \in N(i)} \frac{1}{v_i} \overrightarrow{\Phi}_{ij} s_{ij} = 0$$

with the numerical flux:  $\overrightarrow{\Phi}_{ij} = \frac{1}{s_{ij}} \int_{\partial C_{ij}} \mathcal{F}(U) . \vec{n_{ij}} \, \mathrm{d}s$ Usually, the numerical flux  $\vec{\Phi}_{ij}$  is defined by solving exactly/ approximately a Riemann problem:

$$\begin{cases} \frac{\partial U}{\partial t} + \nabla \cdot (\mathcal{F}(U)) = 0 \\ U(x,t) = \begin{cases} U_i & \text{if } x \in C_i \\ U_j & \text{if } x \in C_j \end{cases} \text{ or } \begin{cases} \frac{\partial U}{\partial t} + \frac{\partial \vec{F}_{\vec{n}}}{\partial \vec{n}} \frac{\partial U}{\partial \vec{n}} = 0 \\ U(x,t) = \begin{cases} U_i & \text{if } \vec{x}.\vec{n} < 0 \\ U_j & \text{if } \vec{x}.\vec{n} > 0 \end{cases}$$

・日・ ・ヨ・ ・ヨ・

## Finite volume discretisation

And we have the numerical flux  $\vec{\Phi}_{ij}$ :

$$\overrightarrow{\Phi}_{ij} = rac{F(U_i) + F(U_j)}{2}.ec{n}_{ij} - \mathcal{D}(U_i, U_j) rac{U_j - U_i}{2}$$

Various choices for  $\mathcal{D}(U_i, U_j)$ :

- $\mathcal{D} = 0$ : centered scheme.
- $\mathcal{D} = |A_{Roe,\vec{n}_{ii}}|$ : upwind scheme.
- $\mathcal{D} = \rho(A)\mathbf{I}$ : Rusanov scheme etc ...

高 とう モン・ く ヨ と

## Roe scheme

Replace the exact nonlinear Riemann problem by a approximate problem linearized between cells i and j

$$rac{\partial U}{\partial t} + A(U_i, U_j, \vec{n}_{ij}) rac{\partial U}{\partial \vec{n}_{ij}} = 0$$

 $A_{Roe,\vec{n}_{ij}}(U_i, U_j) = A(U_i, U_j, \vec{n}_{ij})$  satisfies 3 conditions:

- $A_{Roe,\vec{n}_{ii}}$  is diagonalizable
- **2** Consistency:  $A_{Roe,\vec{n}_{ij}}(U_i, U_i) = \nabla F_{\vec{n}}(U_i)$
- Sonservation:  $(F(U_i) F(U_j)) \cdot \vec{n}_{ij} = A_{Roe, \vec{n}_{ij}} (U_i U_j)$

イロト イポト イラト イラト 一日

## Roe scheme

The Roe's numerical flux:

$$\vec{\Phi}_{ij} = \frac{F(U_i) + F(U_j)}{2} \cdot \vec{n}_{ij} - |A_{Roe,\vec{n}_{ij}}| \frac{U_j - U_i}{2}$$
$$= F(U_i) \overrightarrow{n}_{ij} + A_{Roe,\vec{n}_{ij}}(U_j - U_i)$$
$$= F(U_j) \overrightarrow{n}_{ij} - A_{Roe,\vec{n}_{ij}}^+(U_j - U_i)$$

with |A| the absolute value of A,  $A^+ = \frac{A+|A|}{2}$ ,  $A^- = \frac{A-|A|}{2}$ The final scheme:

$$\frac{U_i^{n+1}-U_i^n}{\Delta t}+\sum_{j\in N(i)}\frac{s_{ij}}{v_i}A^-_{Roe,\vec{n}_{ij}}(U_j-U_i)=0$$

(日) (四) (王) (王) (王)

## The Single-phase Flows

Eq of state:  $p = (\gamma - 1)e\rho$ .

$$\begin{array}{rcl} & & & \rho : \text{ density} \\ & & & \overrightarrow{q} & & \\ & & & \overrightarrow{q} & & \\ & & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & &$$

- T : temperature
- $\nu$  : viscosity

同 と く き と く き と

1 1.

•  $\lambda$  : conductivity

2

## **Numerical Schemes**

$$\frac{\partial U}{\partial t} + \nabla \cdot (\mathcal{F}^{conv}(U)) + \nabla \cdot (\mathcal{F}^{diff}(U)) = 0$$
(3)

*U* the vector of unknown physical quantities  $\mathcal{F}^{conv}(U)$  the flux of convection,  $\mathcal{F}^{diff}(U)$  the flux of diffusion Finite volume formulation

$$\int_{C_i} \frac{\partial U}{\partial t} \, \mathrm{d}\vec{x} + \sum_{j \in \mathcal{N}(i)} \int_{\partial C_{ij}} \left( \mathcal{F}^{conv}(U) \cdot \vec{n_{ij}} + \mathcal{F}^{diff}(U) \cdot \vec{n_{ij}} \right) \, \mathrm{d}s = 0 \quad (4)$$

Set  $U_i(t) = \frac{1}{v_i} \int_{C_i} U(x, t) dx$  and  $U_i^n = U_i(n\Delta t)$ , we have:

$$\frac{U_i^{n+1} - U_i^n}{\Delta t} + \sum_{j \in N(i)} \frac{s_{ij}}{v_i} (\overline{\Phi^{conv}}_{ij} + \overline{\Phi}_{ij}^{diff}) = 0$$
(5)
(6)

・ロン ・回 と ・ ヨ と ・ ヨ と

Use Roe's scheme of the numerical flux of convection  $\overrightarrow{\Phi}_{ii}^{conv}$ :

$$\overrightarrow{\Phi}_{ij}^{conv} = \frac{\mathcal{F}^{conv}(U_i) + \mathcal{F}^{conv}(U_j)}{2} . \vec{n}_{ij} + \mathcal{D}\frac{U_j - U_i}{2} \qquad (7)$$

$$= \mathcal{F}^{conv}(U_i) \overrightarrow{n}_{ij} + A^-(U_i, U_j)(U_j - U_i). \qquad (8)$$

with  $A^- = \frac{A-D}{2}$  and A is a Roe's matrix. For the numerical flux of diffusion  $\overrightarrow{\Phi}_{ij}^{diff}$  on structured meshes:

$$\overrightarrow{\Phi}_{ij}^{diff} = D(U_i, U_j)(U_j - U_i)$$
(9)

Explicit system

$$\frac{U_i^{n+1} - U_i^n}{\Delta t} + \sum_{j \in \mathcal{N}(i)} \frac{s_{ij}}{v_i} \{ (A^- + D)(U^n) \} (U_j^n - U_i^n) = 0$$
(10)

(4回) (注) (注) (注) (注)

## Implicit scheme

Implicit non linear system

$$\frac{U_i^{n+1} - U_i^n}{\Delta t} + \sum_{j \in \mathcal{N}(i)} \frac{s_{ij}}{v_i} \{ (A^- + D)(U^{n+1}) \} (U_j^{n+1} - U_i^{n+1}) = 0$$
(11)

We have the equation: f(U) = 0, with:

$$f(U)|_{i} = \frac{U_{i} - U_{i}^{n}}{\Delta t} + \sum_{j \in N(i)} \frac{s_{ij}}{v_{i}} \{ (A^{-} + D)(U_{i}, U_{j}) \} (U_{j} - U_{i})$$

We solve with the Newton iterative algorithm:

$$f'(U^k)(U^{k+1} - U^k) + f(U^k) = 0$$

- 4 同 6 4 日 6 4 日 6

## Newton scheme

Solve several linear systems to obtain the required solutions:

$$\begin{aligned} \frac{\delta U_i^{k+1}}{\Delta t} &+ \sum_{j \in \mathcal{N}(i)} \frac{s_{ij}}{v_i} \left[ (A^- + D) (U_i^k, U_j^k) \right] \left( \delta U_j^{k+1} - \delta U_i^{k+1} \right) \\ &= -\frac{U_i^k - U_i^n}{\Delta t} - \sum_{j \in \mathcal{N}(i)} \frac{s_{ij}}{v_i} \left[ (A^- + D) (U_i^k, U_j^k) \right] (U_j^k - U_i^k), \end{aligned}$$

where  $\delta U_i^{k+1} = U_i^{k+1} - U_i^k$ . Each Newton iteration requires the numerical solution of the following linear system:

$$\mathcal{A}(\mathcal{U}^k)\delta\mathcal{U}^{k+1} = b(\mathcal{U}^n, \mathcal{U}^k)$$
(12)

where  $\mathcal{U} = (U_1, \ldots, U_N)^t$ .

・ 同 ト ・ ヨ ト ・ ヨ ト

## Table of contents

## 1 Introduction

2 Numerical Scheme



- 4 回 2 - 4 □ 2 - 4 □

## The test cases

- Detonation in a closed box
- Lid driven cavity flows



## Figure: Mesh

ヘロン 人間 とくほど 人間 と

Э

## Initial data



Detonation problem  $\vec{v} = \vec{0}$   $\mathcal{T} = 300K$ Fixed walls  $200 \times 200$  grid

・ロト ・回ト ・ヨト ・ヨト

3

## Initial data

# Velocity X 0 0

## Lid driven cavity $\vec{v} = \vec{0}$ T = 35K3 fixed walls 1 moving wall $50 \times 50$ grid

< □ > < □ > < □ >

## Explicit vs Implicit: Lid driven cavity







### Figure: cfl 1600 nb time steps 1

イロト イヨト イヨト イヨト

CFL	0.5	100	400	800	1600
Number of time steps	3152	16	4	2	1
Time of computation	155.987	3.55	1.079	0.634	0.34

## Upwind vs Centered: Lid driven cavity







Figure: Centered scheme, Stationnary regime

イロト イヨト イヨト イヨト

The centered scheme is much less diffusive and captures the correct solution as opposed to the upwind scheme.

## Scaling strategy

- For a better preconditioning of the matrix, off diagonal entries of the matrix must have a small magnitude
- After applying a similarity transformation with a diagonal matrix  $D_{sca}$  and  $D_{sca}^{-1}$ , all entries of the matrix have the same magnitude.
- Instead of solving system  $\mathcal{A}\delta\mathcal{U} = \mathbf{b}$ , one can rather solve:

$$\tilde{\mathcal{A}}\delta\tilde{\mathcal{U}}=\tilde{\boldsymbol{b}},\tag{13}$$

where  $\tilde{\mathcal{A}} = D_{sca}\mathcal{A}D_{sca}^{-1}$ ,  $\delta \tilde{\mathcal{U}} = D_{sca}\delta \mathcal{U}$  and  $\tilde{b} = D_{sca}b$ .

- System (13) can be resolved more easily using an ILU preconditioner.
- T.H.Dao, M. Ndjinga, F. Magoules, Comparison of Upwind and Centered Schemes for Low Mach Number Flows, *Finite Volumes for Complex Application VI*, Prague, June 6-10 2011.

## Scaling strategy



# Figure: Number of GMRES iterations for the upwind scheme, CFL 1000



Figure: Number of GMRES iterations for the centered scheme. Thu Huyen Dao



Figure: Number of GMRES iterations for the upwind scheme, mesh  $100 \times 100$ 



Figure: Number of Newton iterations for the centered scheme Numerical Solutions of Partial Diffirential Equations

## THANK YOU FOR YOUR ATTENTION!

Thu Huyen Dao Numerical Solutions of Partial Diffirential Equations

イロン イヨン イヨン イヨン